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Lamont Geological Observatory

Technical Report on Seismology

No. 11

Rayleigh Wave Coupling to Atmospheric
Compressional Waves

Lamont Geological Observatory
(Columbia University)
Palisades, New York

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Technical Report No. 11

by

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Frank Press

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The research reported in this document has been made possible through support and sponsorship extended by the Geophysical Research Directorate of the Cambridge Field Station, AMC, U. S. Air Force, under Contract W-28-099 ac-396. It is published for technical information only and does not represent recommendations or conclusions of the sponsoring agency.

January 1951

ABSTRACT

The theory of dispersive Rayleigh waves coupled to atmospheric compressional waves is derived for the case of a solid surface layer. Numerical computation of phase and group velocity curves indicate that an additional branch may be introduced to the dispersion curves as a result of air coupling. Amplitudes of waves propagated according to the various branches are briefly discussed.

INTRODUCTION

Recent experimental and theoretical work has indicated that coupling of surface waves to the atmosphere is not an uncommon phenomena. Press, Crary, Oliver and Katz ⁽¹⁾ identified air coupled flexural waves on a floating ice sheet.

Press and Ewing ⁽²⁾ made use of Lamb's elementary theory ⁽³⁾ to show that coupling between air waves and surface waves of all types is appreciable when the phase velocity of the surface wave is very close to the speed of sound in air. These authors also developed the exact theory for air coupled flexural waves in a floating ice sheet and presented numerical computation of dispersion and relative amplitudes.

An experimental investigation of air-coupling to Rayleigh waves has recently been completed with the cooperation of the Field Research Laboratory of Magnolia Petroleum Company. A paper reporting on these results, entitled "Coupling of Ground Roll to Atmospheric Compressional Waves" by Frank Press and Maurice Ewing will be submitted for publication in "Geophysics" shortly.

Coupling of the atmosphere with hydrodynamic gravity waves is now being investigated.

1. Frank Press, A. P. Crary, Jack Oliver and Sam Katz, "Air-Coupled Flexural Waves", in press. Trans. Amer. Geoph. Union.
2. Frank Press and Maurice Ewing "Theory of Air Coupled Flexural Waves", Geophys. Research Paper No. 6, Cambridge Air Force Research Laboratories, 1950.
3. H. Lamb, "On Waves due to a Travelling Disturbance", with an application to Waves in Superposed Fluids", Phil. Mag. Vol. 31, No. 6, P. 387, 1916.

In this paper, the theory for air coupled Rayleigh waves originating in an impulsive point source in the air, is outlined for the case of a solid surface layer. Numerical computation of dispersion is made for a particular case, the results being applicable for a source in the air or in the ground.

THEORY

The existence of air coupled Rayleigh waves was shown by Bateman ⁽⁴⁾ on the assumption of an homogeneous earth.

Lee investigated the propagation of Rayleigh waves in two solid layers ^(5,6).

We now consider Rayleigh Waves coupled to atmospheric compressional waves for the case of a three layered space formed by air in the half space $z = 0$ to $z = -\infty$, an "upper" solid layer (1) between the planes $z = 0$ and $z = H$ and a "lower" layer (2) between $z = H$ and $z = \infty$. We assume a point source in the air at a distance d above the plane $z = 0$. We denote by $\rho_0, \rho_1, \rho_2, \alpha_0, \alpha_1, \alpha_2, \beta_1, \beta_2$ the densities and velocities of dilatational and shear waves in the air and the elastic media 1 and 2.

Applying the well known method of Lamb ⁽⁷⁾, we represent the horizontal component of displacement, q , and the vertical component, w , by the formulae

$$q = \frac{\partial \varphi}{\partial z} + \frac{\partial^2 \psi}{\partial z \partial z} \quad (1)$$

$$w = \frac{\partial \varphi}{\partial z} + \frac{\partial^2 \psi}{\partial z^2} + \frac{\omega^2}{\beta^2} \psi$$

where r and z are two cylindrical coordinates. Simple harmonic motion of the form $e^{i\omega t}$ has been assumed. The differ-

4. H. Bateman, "Rayleigh Waves", Nat.Acad.Sci.Proced., Vol.24, pp. 315-320, 1938.
5. A. W. Lee, "The Effect of Geological Structure upon Microseismic Disturbance", Mon.Not.Roy.Astron.Soc., (Geophys.Suppl.), Vol. 3, pp. 83-105, 1932.
6. A. W. Lee, "Further Investigation of the Effect of Geologic Structure on Microseismic Disturbance", Mon.Not.Roy.Astron.Soc., Geophys. Suppl. Vol. 3, pp. 238-252, 1934.

ential equations of motion may be transformed to the following system

$$\begin{aligned} (\nabla^2 + \frac{\omega^2}{\alpha_0^2}) \varphi_0 &= 0, \\ (\nabla^2 + \frac{\omega^2}{\alpha_1^2}) \varphi_1 &= 0, \quad (\nabla^2 + \frac{\omega^2}{\beta_1^2}) \psi_1 = 0, \\ (\nabla^2 + \frac{\omega^2}{\alpha_2^2}) \varphi_2 &= 0, \quad (\nabla^2 + \frac{\omega^2}{\beta_2^2}) \psi_2 = 0. \end{aligned} \quad (2)$$

In order to find the functions φ_i and ψ_i which satisfy equations (2), we must specify the boundary conditions. The stresses

$$\rho_{zz} = \lambda \Delta + 2\mu \frac{\partial w}{\partial z} = \lambda \nabla^2 \varphi + 2\mu \frac{\partial w}{\partial z} \quad (3)$$

$$\rho_{zr} = \mu \left(\frac{\partial q}{\partial z} + \frac{\partial w}{\partial r} \right) \quad (4)$$

where λ and μ are Lamé's constants, satisfy the conditions

$$(\rho_{zz})_r = (\rho_{zz})_0, \quad (\rho_{zr})_r = 0 \quad \text{at } z=0 \quad (5)$$

and

$$(\rho_{zz})_z = (\rho_{zz})_r, \quad (\rho_{zr})_z = (\rho_{zr})_r \quad \text{at } z=H \quad (6)$$

If we assume that no voids are formed at the interface between the air and the upper layer, we may write

$$w_r = w_0 \quad \text{at } z=0 \quad (7)$$

and, if a welded connection between the two solid layers is assumed, we have

$$w_z = w_r, \quad q_z = q_r \quad \text{at } z=H. \quad (8)$$

It is also assumed that the displacements vanish at $z = \pm \infty$.

Following Lamb⁽⁸⁾, we introduce two conditions which must be satisfied at the horizontal plane passing through the source ($z = d$),

7. H. Lamb, "On the Propagation of Tremors over the Surface of an Elastic Solid", Phil. Trans. Roy. Soc. Lond., Ser. A. Vol. 203, pp. 1 - 42, 1904.
8. H. Lamb, Ibid.

namely, the pressure must be continuous

$$\rho_0 \frac{\partial \varphi_0'}{\partial t} = \rho_0 \frac{\partial \varphi_0''}{\partial t} \quad \text{at } z = d, \quad \begin{cases} \varphi_0'' \text{ below } z = d, \\ \varphi_0' \text{ above } z = d, \end{cases} \quad (9)$$

and the vertical component of the velocity is discontinuous at the plane $z = d$

$$\frac{\partial \varphi_0'}{\partial z} - \frac{\partial \varphi_0''}{\partial z} = 2YJ(\kappa z) \quad (10)$$

The fundamental solutions of equations (2) satisfying all above conditions must be written in the well known form

$$\varphi_0' = A \exp(\gamma_0 z) J_0(\kappa z), \quad |z| > |d| \quad (11)$$

$$\varphi_0'' = \{B \exp(-\gamma_0 z) + C \exp(\gamma_0 z)\} J_0(\kappa z), \quad |d| \geq |z| \geq 0 \quad (12)$$

$$\varphi_1 = \{D \exp(\gamma_1 z) + E \exp(-\gamma_1 z)\} J_0(\kappa z), \quad 0 \leq z \leq H \quad (13)$$

$$\varphi_2 = F \exp(-\gamma_2 z) J_0(\kappa z), \quad H < z < \infty \quad (14)$$

$$\varphi_3 = \{M \exp(\gamma_3 z) + N \exp(-\gamma_3 z)\} J_0(\kappa z), \quad 0 \leq z \leq H \quad (15)$$

$$\varphi_4 = P \exp(-\gamma_4 z) J_0(\kappa z), \quad H < z < \infty \quad (16)$$

where $J_0(\kappa z)$ is the Bessel function and the positive real or

positive imaginary constants γ_i are given by relations

$$\begin{aligned} \gamma_0^2 &= \kappa^2 - \frac{\omega^2}{\alpha_0^2}, & \gamma_1^2 &= \kappa^2 - \frac{\omega^2}{\alpha_1^2}, & \gamma_2^2 &= \kappa^2 - \frac{\omega^2}{\alpha_2^2}, \\ \gamma_3^2 &= \kappa^2 - \frac{\omega^2}{\beta_1^2}, & \gamma_4^2 &= \kappa^2 - \frac{\omega^2}{\beta_2^2} \end{aligned} \quad (17)$$

in order to satisfy equations (2). Nine arbitrary constants,

A, B, C, \dots, P figuring in the expressions (11)-(16) may be

chosen so that the nine conditions (5), (6), (7), (8), (9) and (10)

are satisfied.

On substituting the functions (11)-(16) in these boundary conditions, we obtain the following system of equations to determine the values of A, B, C, \dots, P :

$$\omega^2 \rho_0 (\beta + C) + (2\mu_1 \kappa^2 - \rho_1 \omega^2) (\mathcal{D} + E) + 2\mu_1 \gamma_3 \kappa^2 (\mathcal{M} - \mathcal{N}) = 0 \quad (18)$$

$$2\gamma_1 (\mathcal{D} - E) + (\gamma_3^2 + \kappa^2) (\mathcal{M} + \mathcal{N}) = 0 \quad (19)$$

$$(2\mu_1 \kappa^2 - \rho_1 \omega^2) (\mathcal{D} e^{\gamma_1 H} + E e^{-\gamma_1 H}) - (2\mu_2 \kappa^2 - \rho_2 \omega^2) \mathcal{F} e^{-\gamma_2 H} \\ + 2\mu_1 \gamma_3 \kappa^2 (\mathcal{M} e^{\gamma_3 H} - \mathcal{N} e^{-\gamma_3 H}) + 2\mu_2 \gamma_4 \kappa^2 \mathcal{P} e^{-\gamma_4 H} = 0 \quad (20)$$

$$2\mu_1 \gamma_1 (\mathcal{D} e^{\gamma_1 H} - E e^{-\gamma_1 H}) + 2\mu_2 \gamma_2 \mathcal{F} e^{-\gamma_2 H} + \mu_1 (\gamma_3^2 + \kappa^2) (\mathcal{M} e^{\gamma_3 H} + \\ + \mathcal{N} e^{-\gamma_3 H}) - \mu_2 (\gamma_4^2 + \kappa^2) \mathcal{P} e^{-\gamma_4 H} = 0 \quad (21)$$

$$\gamma_0 (-\beta + C) - \gamma_1 (\mathcal{D} - E) - \kappa^2 (\mathcal{M} + \mathcal{N}) = 0 \quad (22)$$

$$\gamma_1 (\mathcal{D} e^{\gamma_1 H} - E e^{-\gamma_1 H}) + \gamma_2 \mathcal{F} e^{-\gamma_2 H} + \kappa^2 (\mathcal{M} e^{\gamma_3 H} + \mathcal{N} e^{-\gamma_3 H}) - \kappa^2 \mathcal{P} e^{-\gamma_4 H} = 0 \quad (23)$$

$$\mathcal{D} e^{\gamma_1 H} + E e^{-\gamma_1 H} - \mathcal{F} e^{-\gamma_2 H} + \gamma_3 (\mathcal{M} e^{\gamma_3 H} - \mathcal{N} e^{-\gamma_3 H}) + \gamma_4 \mathcal{P} e^{-\gamma_4 H} = 0 \quad (24)$$

$$A e^{\gamma_0 d} - B e^{-\gamma_0 d} - C e^{\gamma_0 d} = 0 \quad (25)$$

$$\gamma_0 A e^{\gamma_0 d} + \gamma_0 (B e^{-\gamma_0 d} - C e^{\gamma_0 d}) = 2Y \quad (26)$$

Two of the coefficients A, B, ..., P may be easily eliminated. From the two last equations it follows

$$B = \frac{Y}{\gamma_0} e^{\gamma_0 d} \quad (27)$$

and

$$C = A - \frac{Y}{\gamma_0} e^{-\gamma_0 d} \quad (28)$$

Therefore, the equations (18)-(24) take the form

$$a_1 A + d_1 \mathcal{D} + e_1 E + m_1 \mathcal{M} + n_1 \mathcal{N} = -2\rho_0 \omega^2 \frac{Y}{\gamma_0} \sinh(\gamma_0 d) \\ d_2 \mathcal{D} + e_2 E + m_2 \mathcal{M} + n_2 \mathcal{N} = 0 \\ d_3 \mathcal{D} + e_3 E + m_3 \mathcal{M} + n_3 \mathcal{N} + f_3 \mathcal{F} + \rho_3 \mathcal{P} = 0 \\ d_4 \mathcal{D} + e_4 E + m_4 \mathcal{M} + n_4 \mathcal{N} + f_4 \mathcal{F} + \rho_4 \mathcal{P} = 0 \\ a_5 A + d_5 \mathcal{D} + e_5 E + m_5 \mathcal{M} + n_5 \mathcal{N} = -2Y \cosh(\gamma_0 d) \quad (29)$$

$$d_6 D + e_6 E + m_6 M + n_6 N + f_6 F + \rho_6 P = 0$$

$$d_7 D + e_7 E + m_7 M + n_7 N + f_7 F + \rho_7 P = 0$$

Since the determinant of these seven equations is not identically equal to zero we can find definite values of the coefficients A, B, ... P. We can then apply the method of Lamb (9) and generalize the discontinuity of vertical velocity using the Fourier-Bessel integral by taking $Y = kdk$ and integrating with respect to k from 0 to ∞ . Then we can obtain solutions satisfying all conditions including the requirements for a point source. It may be difficult to evaluate the integrals representing the solutions, since the quantities A, B, ... P are complicated, owing to the high order of the determinant.

We restrict ourselves at this point to the analysis of the frequency equation which is given by the condition that the above determinant is equal to zero.

Since the coefficients a, d, ... of the system (29) depend on the elastic constants and on the quantities ρ_i , α_i , β_i and γ_i which may be expressed as functions of the phase velocity, $c = \omega/\kappa$, this determinant may be considered as a function of the phase velocity c and of the frequency $f = \kappa c / 2\pi$. Equating the determinant to zero, we, therefore, obtain an equation which defines an implicit relationship between frequency and the phase velocity.

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Rewriting the frequency equation, we omit all factors which can-not be equal to zero and transform the remaining determinant to reduce the number of elements. After these transformations, the frequency equation takes the form:

$$\begin{pmatrix}
 1 & \frac{2\mu_1\gamma_3\kappa^2}{\rho_0\omega^2\cosh(\gamma_1H)} & 0 & 0 & 0 \\
 0 & \frac{2\gamma_1}{\sinh(\gamma_1H)} & \frac{2\kappa^2\beta_1^2 - \omega^2}{\beta_1^2\cosh(\gamma_3H)} & 0 & 0 \\
 0 & 0 & 0 & \rho_2\omega^2 + 2(\mu_1 - \mu_2)\kappa^2 & 2(\mu_1 - \mu_2)\kappa^2 \\
 0 & -\rho_1\omega^2 & -\rho_1\omega^2 & 0 & -\rho_1\omega^2 - \rho_1\omega^2 \\
 0 & 0 & 0 & -\rho_1\omega^2 & -\rho_1\omega^2 - \rho_1\omega^2 + \rho_2\omega^2 \\
 0 & -\frac{2\mu_1\kappa^2 - \rho_1\omega^2}{\rho_0\omega^2\cosh(\gamma_1H)} & 0 & \frac{-\omega^2}{2\gamma_0\cosh(\gamma_3H)\beta_1^2} & \frac{-2\mu_1\gamma_3\kappa^2}{\rho_0\omega^2\sinh(\gamma_3H)} \\
 0 & 0 & \gamma_1\tanh(\gamma_1H) & \gamma_1\coth(\gamma_1H) & \kappa^2 \\
 0 & 0 & 1 & \gamma_3\tanh(\gamma_3H) & \gamma_3\coth(\gamma_3H) - 1
 \end{pmatrix} = 0 \quad (30)$$

Developing the determinant, we put

$$V = \frac{c}{\beta_1} \quad (31)$$

and

$$\begin{aligned} n_0 &= \sqrt{1 - V^2 \frac{\beta_1^2}{\alpha_0^2}}, \quad n_1 = \sqrt{1 - V^2 \frac{\beta_1^2}{\alpha_1^2}}, \quad n_2 = \sqrt{1 - V^2 \frac{\beta_1^2}{\alpha_2^2}}, \\ n_3 &= \sqrt{1 - V^2}, \quad n_4 = \sqrt{1 - V^2 \frac{\beta_1^2}{\beta_2^2}} \end{aligned} \quad (32)$$

Introducing Lee's notations ¹⁰

$$\begin{aligned} X &= \frac{\rho_2}{\rho_1} V^2 - 2 \left(\frac{\mu_2}{\mu_1} - 1 \right) \\ Y &= V^2 + 2 \left(\frac{\mu_2}{\mu_1} - 1 \right) = V^2 + W \\ Z &= \frac{\rho_2}{\rho_1} V^2 - V^2 - 2 \left(\frac{\mu_2}{\mu_1} - 1 \right) = X - V^2 \\ W &= 2 \left(\frac{\mu_2}{\mu_1} - 1 \right) \end{aligned} \quad (33)$$

we put

$$G_1 = XZ - n_2 n_4 WY, \quad G_2 = Z^2 - n_2 n_4 Y^2, \quad G_3 = n_2 n_4 W^2 - X^2 \quad (34)$$

and

$$\begin{aligned} \ell_0 &= 4(2-V^2)G_1 \\ \ell_1 &= (2-V^2)^2 \cdot \frac{1}{n_1 n_3} G_2 - 4n_1 n_3 G_3 - \frac{\rho_0 \rho_2}{\rho_1^2} \frac{n_1 n_4}{n_0 n_3} V^8 \\ \ell_2 &= -(2-V^2)^2 \frac{\rho_2}{\rho_1} \frac{n_2}{n_1} V^4 + \frac{4\rho_2}{\rho_1} n_1 n_4 V^4 + \frac{\rho_0}{\rho_1} \frac{n_1}{n_0} V^4 G_3 \quad (35) \\ \ell_3 &= -(2-V^2)^2 \frac{\rho_2}{\rho_1} \frac{n_4}{n_3} V^4 + \frac{4\rho_2}{\rho_1} n_2 n_3 V^4 + \frac{\rho_0}{\rho_1} \cdot \frac{1}{n_0 n_3} V^4 G_2 \\ \ell_4 &= (2-V^2)^2 G_3 - 4G_2 - \frac{\rho_0 \rho_2}{\rho_1^2} \frac{n_2}{n_0} V^8 \end{aligned}$$

The frequency equation then takes the form

$$\begin{aligned} \ell_0 + \ell_1 \sinh(n_1 \kappa H) \sinh(n_3 \kappa H) + \ell_2 \sinh(n_1 \kappa H) \cosh(n_3 \kappa H) + \\ + \ell_3 \cosh(n_1 \kappa H) \sinh(n_3 \kappa H) + \ell_4 \cosh(n_1 \kappa H) \cosh(n_3 \kappa H) = 0 \end{aligned} \quad (36)$$

The last terms of the coefficients ℓ_i having the factors ρ_0 and $1/n_0$ represent the influence of the air.

For numerical computations, it was assumed that Poisson's ratio $\sigma = 0.25$ for both solid layers, i.e. $\lambda_1 = \mu_1$ and $\lambda_2 = \mu_2$.

The following data were used:

$$\alpha_0 = 1070 \text{ ft/sec}, \beta_1 = 800 \text{ ft/sec}, \frac{\beta_2}{\beta_1} = 3.14, \\ \frac{\rho_2}{\rho_1} = 1.39, \frac{\rho_0}{\rho_1} = 0.001, \frac{\mu_2}{\mu_1} = 13.77.$$

These values were chosen as most representative of near surface conditions often encountered in seismic prospecting. It is obvious that air coupling effects are negligible when $.9194\beta_1 > \alpha_0$ since $c > \alpha_0$ for this case, and the air coupling term of the frequency equation which contains the factor $\rho_0/\rho_1 n_0$ is very small.

In the case of air coupled Rayleigh waves, real values of kH must correspond to the interval

$$.9194 \leq V \leq \frac{\alpha_0}{\beta_1}$$

The upper limit is equal in this case, to 1.3375 ($= \frac{1070}{800}$).

For larger values of V , the roots of the frequency equation become complex. We have computed the real and imaginary parts of these roots. They are given in Table II. All real roots computed, and the real parts of complex roots, are given in Table I. The roots were computed by successive approximations, using Lee's computations to obtain the first approximation. It may be remarked that the values of L/H as given by Lee to two or three figures, lead to values of kH which may differ, by some units of

the third figure, from the more exact values computed with five figures directly from the frequency equation. Group velocity U was obtained by graphical differentiation of the phase velocity curve, using the familiar equation

$$U = c + \kappa \frac{dc}{d\kappa}.$$

The phase velocity curve in the case of air coupled Rayleigh waves differs very little from the curve given by Lee until the neighbourhood of the critical point $V = 1.3375$ is reached (Figure I). At this point, it deviates to the left and intersects the V -axis at a point

$$1.3374 < V < 1.3375.$$

The real part of complex roots above the critical value is very close to the corresponding roots of the frequency equation without air connected terms. But it deviates to the right in the neighbourhood of the critical value and "ends" at the point $\kappa H = 4.2515$ of the line $V = 1.3375$.

Results of these computations are presented in dimensionless form in Figure I where c/B_1 and U/B_1 are plotted against κH . The heavy lines indicate where atmospheric influence is negligible and the results are similar to those obtained by Lee. The dashed lines represent new branches introduced by air coupling.

It is well known that the velocities and periods of waves propagated through a dispersive medium can be obtained from the corresponding group velocity curve. To obtain the amplitudes of waves corresponding to the different branches of the group velocity curve, one must compute excitation functions which

depend upon the nature and position of the source, the location of the receivers, and implicitly on the roots of the frequency equation. Although the mathematical procedure is straightforward, the numerical work required is extremely lengthy. We can, therefore, discuss the frequencies and velocities of Rayleigh waves coupled to the atmosphere, but the relative amplitudes of waves for different source and receiver locations cannot be given. Existing calculations for air coupling to another type of surface wave can be used, however, to infer something about relative amplitudes.

The group velocity curve in Figure I is divided into branches I, II, III, each of which represents a different train of waves. Branch I corresponds to the dispersive train of Rayleigh waves observed on seismograms of earthquakes. Branch I also accounts for the dispersive Rayleigh waves usually associated with ground roll. These waves first appear as long period arrivals travelling with the speed of Rayleigh waves in the bottom layer, $U = .9194B_2$. Succeeding waves gradually decrease in period since kH increases as the group velocity decreases. Waves continue to arrive with decreasing period until a time corresponding to propagation at the minimum value of group velocity. From the analogous theory referred to above, we would expect waves propagated according to branch I to predominate for a source located within the solid layers recorded ^apickup on the solid layer. Waves with group velocity values near the minimum in Branch I have

phase velocities approaching the speed of sound in air from the side $c > \alpha_0$. These waves are attenuated since κH is complex and has an increasingly large imaginary component as $c \rightarrow \alpha_0$ (Table II).

No significance should be attached to the occurrence of a minimum value of group velocity near the critical point $c = V_0$. Had we chosen other values for the elastic constants of the layers, the phase velocity corresponding to the minimal group velocity could have been much different from V_0 .

Branch II represents a dispersive train of waves beginning as a high frequency arrival at a time corresponding to propagation with the velocity of Rayleigh waves in the surface layer. The frequency of these waves decreases as time progresses until the time corresponding to propagation at the minimum group velocity when the waves of Branch I and Branch II merge to form a single train of waves having a discrete frequency.

Branch III represents an additional train introduced by coupling of Rayleigh waves to atmospheric compressional waves. This train begins at a time corresponding to propagation at the speed of sound in air and continues with almost constant frequency until the time $t = r/.44B_1$. The phase velocity of these waves should be close to the speed of sound in air. From experimental and theoretical results referred to earlier, we might expect these waves to be prom-

inent for a source in the air recorded by a pickup on the ground, and for a source within the ground recorded by a microphone in the air. There is an additional branch with dispersion features similar to Branch III, corresponding to the complex phase velocities whose real parts are greater than, but close to α .

Higher modes of propagation exist at correspondingly higher frequencies.

CONCLUSIONS

The existence of a surface layer in which the speed of Rayleigh waves is less than the speed of sound in air introduces a new branch to the dispersion curves, corresponding to a train of approximately constant frequency waves beginning with the arrival of the air wave and continuing to a time depending on the distance and the elastic constants of the layers. It is probable that these new waves are especially prominent for a source within the air recorded with a seismograph and for a source within the ground recorded with a microphone.

TABLE I

$V = c/B_1$	LEE'S kH	kH
0.952	5.15	4.753
.992	3.652	3.840
1.10	2.856	2.884
1.28	2.273	2.204
1.30	2.207	2.148
1.32	2.144	2.099
1.336	2.098	2.045
1.337	2.095	2.024
1.3374	2.094	1.977
$1.3374 < V_o < 1.3375$		0
1.3375		4.2515
1.3376	2.094	2.07 ²⁾
1.34	2.06 ¹⁾	2.07 ²⁾
1.38	1.978	1.979 ²⁾
1.40	1.928	1.936 ²⁾
1.41	1.904	
1.65	1.532	
1.98	1.122	
2.15	.938	
2.30	.806	
2.48	.648	
2.53	.610	
2.64	.462	
2.73	.294	
2.81	.143	
2.89	0	

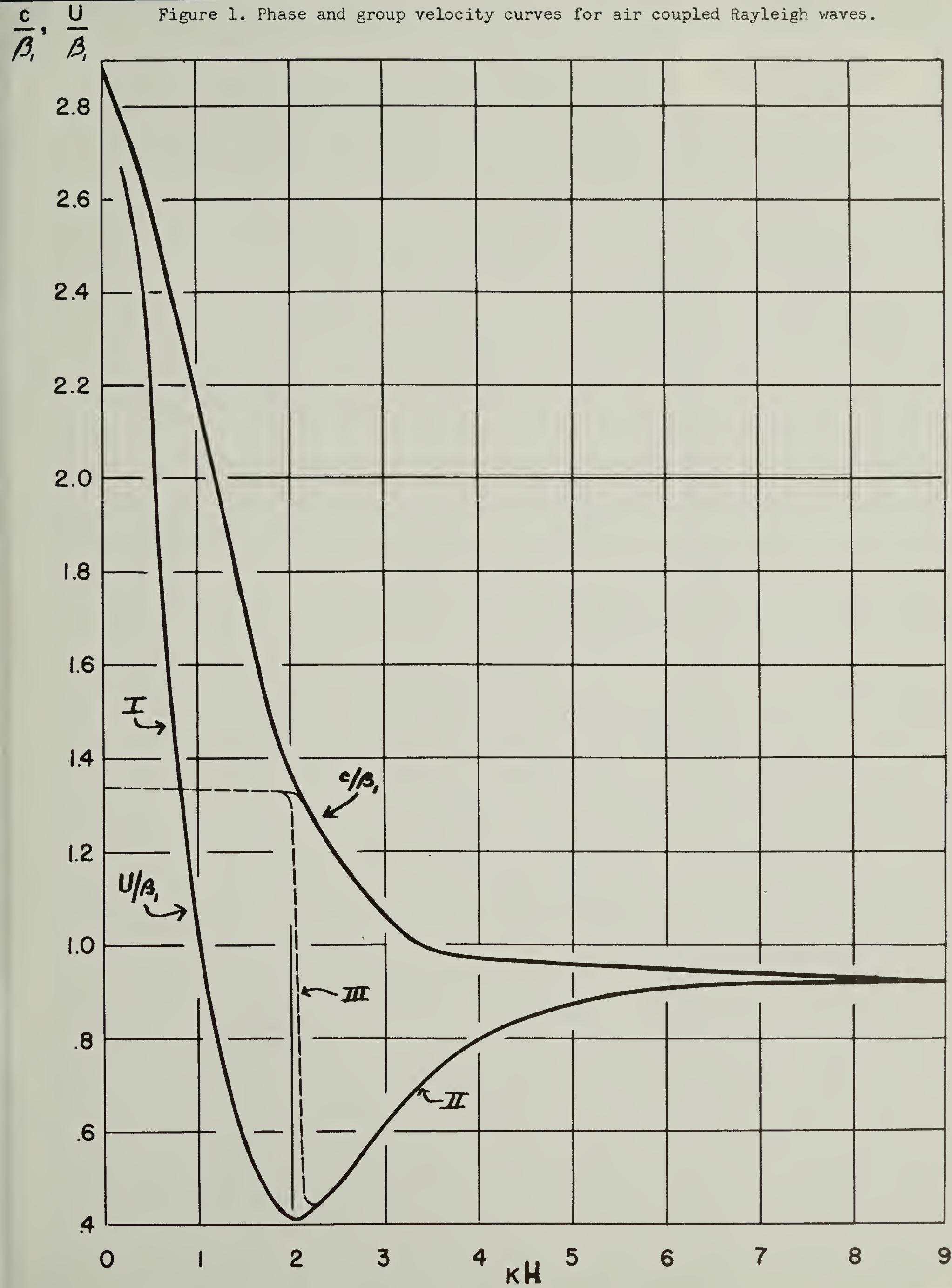
1. This is a more exact value than that obtained
from Lee's data (2.086)

2. Real part

TABLE II

V	kh
—	—
1.3375	4.252
1.3376	2.07 + .08 i
1.34	2.07 + .019 i
1.38	1.98 + .006 i
1.40	1.94 + .001 i

Figure 1. Phase and group velocity curves for air coupled Rayleigh waves.



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